

METHOD AND DEVICE FOR ADAPTIVELY CONTROLLING POWER

Background Information

5 The present invention is directed to a method and a device for adaptively controlling power in accordance with the definition of the species set forth in the independent Claims 1 and 8.

10 In the automotive sector, systems are already in use or still in development, which measure the distances and velocities of objects around one's own vehicle by using microwaves and applying the radar principle. These objects can be vehicles which are actively taking part in the highway traffic as well or, however, be some sort of obstacles on or near the road. Keyless remote-entry systems for vehicles (keyless entry/comfort entry/keyless go systems) also make use of these

15 technologies. In the known systems, high-frequency energy is radiated in a frequency range in the gigahertz range, at a mid-frequency of 24,125 GHz and with a two-way bandwidth of several GHz. Typical antennas have a directional characteristic of 80 degrees * 20 degrees. In practice, the

20 transmission range is about 20 m. The risk inherent in such systems is that unacceptably high signal levels occur, even in frequency ranges that have been blocked in favor of other services. Examples are frequency ranges that are reserved for radio astronomy or also for radio relay services. Unacceptably

25 high signal levels can occur, for example, when a substantial number of the above-mentioned systems, for example several hundred, are simultaneously put into operation. This can be the case, for example, when a large number of vehicles are moving on multilane urban streets. Similar problems arise in

large parking lots at sports facilities or shopping centers when, for example, after a big event ends, hundreds of vehicles start moving at the same time and leave the parking lot. For the most part, these problems only occur when the
5 vehicles are at standstill or traveling at a relatively slow speed. This is because, at higher speeds, the distances between the vehicles increase again, and the vehicle density decreases correspondingly. Furthermore, the spatial proximity of many sensors also causes heavy mutual interference, which,
10 when working with adaptive sensors, increasingly leads to additional measurements being taken, although some objects have actually already been reliably detected.

From German Patent Application DE 100 65 521 of the applicant, a method and a device for detecting moving or stationary
15 objects using radar radiation are known, in particular for use in motor vehicles, where, in order to detect objects, pulse-modulated carrier waves are radiated, whose reflected portions are then received and evaluated. In this context, by transmitting an unmodulated carrier in the time intervals
20 between two adjacent pulses, a Doppler measurement can additionally be performed, thereby enabling a reliable velocity measurement to be taken.

From the still to be published Patent Application R. 40543 of the applicant, a method is also known for detecting
25 irregularities when receiving signals. In response to such irregularities, the transmitting branch is switched off. Thus, no more transmission signals are emitted by the transmitting antenna. However, correlation pulses from a pulse transmitter continue to be transmitted to the receiving branch of the
30 radar sensor. If it turns out in the process that object information is still received, then an illusory object must be inferred.

Summary of the Invention

The present invention starts out from the realization that the mentioned problems may be avoided or at least minimized by using an adaptive power control. As soon as it becomes
5 apparent that the interference is getting out of hand due to a heavy traffic density, an appropriate power adaptation is carried out. Once objects have been reliably detected, the measurement repetition rate may preferably be reduced. In addition, the possible detection range does not need to be
10 utilized up to the maximum value, rather, it may be stopped once a limit to be regarded as useful is reached, such as of two to five detected objects, especially as the power requirement increases with the fourth power of the distance. Provided that a ground speed is measurable, at a low speed of
15 less than about 20 to 40 km/h or, however, at standstill and in the case of far away objects, the power may likewise be reduced by limiting the average power, the measurement repetition frequency, or the maximum distance. The relatively low speed makes it unlikely that objects would appear
20 unexpectedly. If necessary, however, a measurement may also be made in-between, up to the first object, in order to make this space safe as well and thereby enhance the safety on the whole. The speed information may be obtained quite advantageously from the wheel speeds, from a radar measurement
25 which records the ground speed, or from an SRR measurement by estimating stationary objects. While the first two mentioned methods lead to very reliable results, the last-mentioned method additionally requires an exact classification into illusory objects, on the one hand, and tangible moving
30 objects, on the other hand, to attain reliable results. Since in situations of high traffic density and, thus, a high concentration of sensors, the interfering influences increase,

but these may be recognized, however, the present invention also makes it possible to adaptively reduce the power within a relatively short distance, provided that reliably detected objects exist. The present invention makes it possible for the transmitting power to be reduced, thereby facilitating an approval in conformance with UWB criteria. By reducing the transmitting power, the interference immunity may be further enhanced. This means that there is less mutual interference among adjacent vehicles. The reduced transmitting power leads to a lower current consumption, which is beneficial in terms of energy usage. Also, because of the reduction in load, one can expect a longer service life. First estimations showed that, by applying the approach of the present invention, assuming a maximum distance of 20 m and a breaking off of the emissions in the distance stages 5m, 10m or 15 m, the average power could be reduced by 30 db, 15 db, and 6 dB, respectively. Consequently, the spectral density is, of course, also lowered. In addition, the transmitted power could also be lowered by approximately 6 to 20 dB.

Advantageous and practical embodiments, as well as further refinements of the present invention are characterized in the dependent claims.

Brief Description of the Drawing

The present invention is explained below with reference to the specific embodiments illustrated in the drawing, whose figures show:

- Figure 1 a radar device of the related art;
- Figure 2 a motor vehicle having radar devices;
- Figure 3 in a diagram, a radar signal of a radar device;
- Figure 4 in a diagram, radar signals having interference of varying intensity;

Figure 5 a block diagram of a radar device;
Figure 6 a first flow chart illustrating the reduction
of power;
Figure 7 a second flow chart illustrating the reduction
5 of power.

Detailed Description

In a block diagram, Figure 1 shows a radar device having a correlation receiver as known from the related art. A pulse generator 2 induces a transmitting device 1 to emit a
10 transmitted signal 6 via an antenna 4. Transmitted signal 6 impinges on a target object 8, where it is at least partially reflected, and returns to receiver 14. Received signal 10 is received by antenna 12. In this context, antenna 12 and antenna 4 may be identical and be switched between
15 transmitting and receiving operation. Upon receipt of received signal 10 by antenna 12, received signal 10 is routed to receiver 14 and subsequently fed via a filter device having A/D conversion 16 to an evaluation device 18. An exceptional feature of such a radar device, which has a correlation
20 receiver, is that receiver 14 receives a reference signal 20 from pulse generator 2. Received signals 10 received by receiver 14 are mixed in receiver 14 with reference signal 20. The correlation operation makes it possible to infer the
25 temporal delay from emission of a radar signal until receipt of a radar signal reflected off of a target object.

It is possible to operate a plurality of substantially identical, for example between 4 and 16 radar sensors on one vehicle. This is clearly shown on the basis of Figure 2, which
30 illustrates a motor vehicle 20 having a multiplicity of radar sensors 21. Radar sensors 21 are preferably interconnected via

a bus concept and to control devices. Thus, a device 24 for providing a park distance control and for detecting a blind spot, a device 26 for the precrash function, as well as a device 28 for facilitating travel in stop-and-go traffic are provided, in particular.

In a diagram, Figure 3 shows a typical radar signal which is transmitted by a radar device working in the short range. When working with a radar device of this kind, high-frequency energy is radiated in a frequency range in the gigahertz range, at a mid-frequency of 24,125 GHz and with a two-way bandwidth of several GHz.

In a diagram, Figure 4 shows typical received signals which have been picked up by a radar device working in the short range. The characteristic curve of first received signal ES1 shown in the upper part of the diagram is substantially undisturbed. The characteristic curve of second received signal ES2 shown in the middle area of the diagram is influenced by a strong interference, which could be caused by an FMCW radar. Third received signal ES3 illustrated in the lower part of the diagram is affected by a very strong interference of the same type.

Figure 5 shows a block diagram of a radar device 520 which is provided for monitoring the near zone around a motor vehicle. A control device 522 supplies energy to radar device 520. Thus, for example, control device 522 supplies an input voltage of 8 V for radar device 520. This input voltage is fed to a DC/DC converter 524 which makes available a supply voltage of, for example, 5 V for the components of radar device 520. Radar device 520 also includes a local oscillator 526 which produces a carrier frequency of preferably 24 GHz. This local oscillator is supplied with a bias voltage

generated by a converter 530, which is driven by pulses produced by a clock-pulse generator 528. The pulses produced by clock-pulse generator 528, which may have a frequency of a few MHz, in particular 5 MHz, are used to modulate the carrier signal supplied by local oscillator 526. This modulation is carried out in the transmitting branch of radar device 520 by a switching element 532 which is controlled by a pulse shaper 546. Pulse shaper 546, in turn, is likewise driven by the clock frequency of clock-pulse generator 528. The pulsed signals generated in this manner are radiated by an antenna 534. In the case that the signals emitted by antenna 534 are reflected off of a target object, for example, the reflected signals are received by an antenna 536. Once the received signals are amplified in an amplifier 538, the signals are fed to two mixers 540 and 542. First mixer 540 then emits a so-called I-signal, while second mixer 542 outputs a 90° out-of-phase Q-signal. In mixers 540, 542, the received signals are mixed with the pulsed signals of local oscillator 526, this pulsing taking place via a switch 544. Switch 544 is driven by a pulse generator 548 which outputs delayed pulses. For example, pulses output by pulse generator 548 are delayed by a time period t with respect to the pulses from pulse generator 546. This delay is effected by a delay circuit 500. The duration of the delay of delay circuit 500 is influenced via a microcontroller 552, which preferably includes a digital signal processor. This is accomplished via a first analog output 554 of microcontroller 552. Via a second analog output 560, the I- or Q-signals processed by an amplifier 556 are influenced by another, preferably variable amplification in amplifier 558. This amplifier 558 is controlled by a second analog output 560 of microcontroller 552. The output signal from amplifier 558 is fed to an analog input 562 of microcontroller 552. Microcontroller 552 communicates via an

input/output bus 564 with control device 522. Radar device 520 also includes a so-called notch filter 566, which is suited, in particular, for suppressing monochromatic or nearly monochromatic interference signals. Also provided are a PLL circuit 568 and a further mixer 570. The frequency of an interference signal may be advantageously determined by tuning PLL circuit 568.

Accordingly, using the above-described device, it is possible to ascertain interference in the received signal and to classify the type of interference. At this point, as soon as it is determined that the detected interference is attributable to a too great traffic density, an appropriate power adaptation, which may contribute to a reduction in the interference, is carried out in accordance with the present invention. Once objects have been reliably detected, the measurement repetition rate may preferably be reduced. Since fewer radar signals are emitted as a result, the probability of interference being caused is also reduced. In addition, it is not necessary to utilize the possible detection range up to the maximum value. Rather, it may be stopped once a limit to be regarded as useful is reached, such as of two to five detected objects, especially as the power requirement increases with the fourth power of the distance. This is clarified in the following with reference to the flow chart illustrated in Figure 6. In a first step 60, radar device 520 is operated in normal operation. In this normal operation, measurements are taken at regular intervals up to a maximum range of about 20 m. In a step 61, it is checked whether objects have been detected within a relatively short distance. If this is not the case, alternative path 61a is selected, and the normal operation is continued in accordance with step 60. If, on the other hand, objects are detected within the

relatively short distance, alternative path 61b is selected, and power is reduced in accordance with step 62 in that measurements are still only taken up to a limiting distance of n m, where $n < 20$ m. First estimations showed that, by
5 applying the approach of the present invention, assuming a maximum distance of 20 m and a forced termination of the emissions in the distance stages 5m, 10m or 15 m, the average power could be reduced by 30 db, 15 db, and 6 dB, respectively. Consequently, the spectral density is, of
10 course, also lowered. In addition, the transmitted power could also be lowered by approximately 6 to 20 dB.

An alternative approach for reducing power is clarified with reference to the flow chart shown in Figure 7. In a first step 70, radar device 520 is operated in normal operation. In this
15 normal operation, measurements are taken at regular intervals up to a maximum range of about 20 m. In a subsequent step 71, it is checked whether the vehicle is stationary or whether it is moving at a relatively low speed. If this is not the case, alternative path 71b is selected, and the normal operation is
20 continued in accordance with step 70. If, however, only a low speed of less than about 20 to 40 km/h is measured, or, however, it is determined that the vehicle is stationary, alternative path 71a may be taken to arrive at step 72. In this step 72, it is checked, in turn, analogously to step 61
25 in the previously described exemplary embodiment, whether objects have been detected in a distance shorter than 20 m. If this is the case, alternative path 72a is selected, and power is reduced in accordance with step 73 in that measurements are still only taken up to a limiting distance of n m, where $n <$
30 20 m. This yields the above-mentioned advantages. The relatively low speed makes it unlikely that objects would appear unexpectedly. If necessary, however, a measurement may

also be made in-between, up to the first object, in order to make this space safe as well and thereby enhance the safety on the whole. If this is not the case, alternative path 72b is selected, and the normal operation is continued in accordance with step 70.

The speed information may be obtained quite advantageously from the wheel speeds, from a radar measurement which records the ground speed, or from an SRR measurement by estimating stationary objects. While the first two mentioned methods lead to very reliable results, the last-mentioned method additionally requires an exact classification into illusory objects, on the one hand, and tangible moving objects, on the other hand, to attain reliable results. Since in situations of high traffic density and, thus, a high concentration of sensors, the interfering influences increase, but these may be recognized, however, the present invention also makes it possible to adaptively reduce the power within a relatively short distance, provided that reliably detected objects exist. The present invention makes it possible for the transmitting power to be reduced, thereby facilitating an approval in conformance with UWB criteria. By reducing the transmitting power, the interference immunity may be further enhanced. This means that there is less mutual interference among adjacent vehicles. The reduced transmitting power leads to a lower current consumption, which is beneficial in terms of energy usage. A longer service life may be expected as well, due to the reduction in load.

Reference Numeral List

1	transmitting device
2	pulse generator
4	antenna
6	transmitted signal
8	target object
10	received signal
12	antenna
14	receiver device
16	filter device having A/D conversion
18	evaluation device
19	reference signal
20	motor vehicle
21	radar sensor
24	device for park distance control
26	device for stop and go traffic
28	device for precrash function
60	step
61	step
61a	path
61b	path
62	step
70	step
71	step
71a	path
71b	path
72	step
72a	path
72b	path
73	step
74	step
ES1	received signal
ES2	received signal

ES3 received signal
500 delay circuit
520 radar device
522 control device
524 DC/DC converter
526 local oscillator
528 clock-pulse generator
530 converter
532 switch
534 antenna
536 receiving antenna
538 amplifier
540 mixer
542 mixer
544 switch
546 pulse generator
548 pulse generator
552 microcontroller
554 analog output
556 amplifier
558 amplifier
560 analog output
562 analog input
564 input/output bus
566 notch filter
568 PLL circuit
570 mixer